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HIGH VELOCITY COMPACTION OF CARBON COMPOSITIONS

M.N. Samodurova, samodurovamn@susu.ru, *L.A. Barkov*, barkovla@susu.ru, *Yu.S. Latfulina*, latfulina174@gmail.com South Ural State University, Chelyabinsk, Russian Federation

> High velocity compaction of metal, ceramic and other powders have no widespread industrial application at the present time. Carrying out a large number of experiments with processes of high velocity compaction with powders of non-ferrous, ferrous metals, ceramics and polymers - showed that formation with speeds of the ram tester more than 1-2 m/s, causes the following adverse effects: pressing of gases and vapors of the liquids containing in initial powders and destruction of the specimens. In Chelyabinsk there are several large-scale enterprises ("Electrode Plant", "Electrometallurgical Integrated Plant", Plant "Grafitoplast", branch of "Doncarb Graphite", "Uglegraphite", "Carbon Material Plant" and others), which produce a brand range of products from carbon compositions. Scientists from Resource Centre of Special Metallurgy of South Ural State University (RCSM of SUSU) carried out the theoretic, technologic and experimental investigations for these enterprises. This article is devoted to the analysis of the experimental studies on devices of the Swedish company HY-DROPULSOR and the American company Instron. Foreign researchers established values of devices striker pin kinetic energy at which density of specimens comes nearly to theoretical, but, unfortunately, without indication of powder compositions, kind of specimens pressing and also strikers and specimens masses, their density at various values of speed and mass of strikers. Therefore the aim of the article is studying processes of High Velocity Compaction providing different indications of powder compositions containing graphite and optimized strikers and specimens masses, strikers speed.

> *Keywords: high velocity compaction; carbon compositions; granulo-morphological research; HYDROPULSOR press.*

Granulo-morphological research

For granulometric and morphological analysis of the powder composites together with the standard procedure [1-8], were used the methods providing usage of a granulo-morphometer ALPAGA 500 NANO and Electron Microscope Tescan VEGA-II. The granulo-morphometer ALPAGA 500 NANO has an exclusive software Callisto product of the company OCCHIO (Belgium) allows to measure the diameter of the mesh aperture, roundness, elongation and other parameters of the particles with the dimensions from 0.5 to 2500 µm. The specimen preparation is done by placing the particles on the slide through the aperture in the vacuum chamber by making a slight (within 0.1 bar) change of pressure. The diameter of the mesh aperture is a minimum diameter of its hole through which a particle can pass. Roundness is a parameter characterizing departure of the particle form from a perfectly round one. Elongation of the powder particles is a normalized ratio of ellipsoid semi-axis of Lagrange inertia.

Compositions of powder mixtures studied are given in Table 1.

Graphite was obtained from electrode scrap of Chelyabinsk Electrode Plant by ball milling, the particle size is from 1 μ m to 5 mm.

The binder is powdered phenolformaldehyde novolac type resin that has 6–9% of urotropine mass fraction according to Specification Requirements.

Copper electrolytic powder used in composition No. 3, has a bulk density of $1.25-2.00 \text{ g/cm}^3$. In compositions No. 4 and 5 a petroleum coke with the ash content is not more than 0.5 %, was used as an additive.

Powder of zinc stearate, zinc mass fraction does not exceed 4 %, was used in Composition No. 5 as a lubricant between graphite and binding particles.

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| Mixture Number | Graphite, % | Binding, % | Copper, % | Coke, % | Zinc stearete, % |
|----------------|-------------|------------|-----------|---------|------------------|
| 1 | 100 | — | — | - | — |
| 2 | 86 | 14 | — | — | _ |
| 3 | 76 | 14 | 10 | _ | _ |
| 4 | 71 | 14 | _ | 15 | _ |
| 5 | 71 | 14 | — | 10 | 5 |

Compositions of powder mixtures

Results of granulo-morphological research

Results of the granulometric and morphological analyses are given in Tables 2, 3 and 4. Cumulative particle size distribution in powder composites to the mesh aperture diameter is given in Table 2. Thus, for example, for composition No. 1 the minimum mesh aperture diameter is 0.96 μ m, and maximum one is 95 μ m. The part of the particles with mesh aperture diameter up to 13 μ m is 5 %, with mesh aperture diameter up to 18 μ m – 10 %, up to 21 μ m – 16 %, up to 26 μ m – 25 %, up to 40 μ m – 50 % etc, up to 94 μ m – 95 %.

Table 2

Table 3

| Mesh aperture | diameter, | μm | |
|---------------|-----------|----|--|
|---------------|-----------|----|--|

| Mixture number | Average | Minimum | P5 | P10 | P16 | P25 | P50 | P75 | P84 | 06d | P95 | Maximum |
|-------------------|---------|---------|----|-----|-----|-----|-----|-----|-----|-----|-----|---------|
| 1 | 47 | 0,96 | 13 | 18 | 21 | 26 | 40 | 65 | 77 | 85 | 94 | 95 |
| 2 | 32 | 0,96 | 8 | 10 | 12 | 15 | 22 | 40 | 57 | 72 | 86 | 99,8 |
| 3 | 34 | 0,96 | 9 | 11 | 14 | 17 | 26 | 46 | 56 | 72 | 81 | 87 |
| 4 | 33 | 0,48 | 9 | 12 | 15 | 20 | 31 | 44 | 48 | 54 | 64 | 78 |
| 5 | 33 | 0,48 | 9 | 12 | 15 | 18 | 28 | 45 | 53 | 59 | 75 | 76 |

| Mixture number | Average | Minimum | P5 | P10 | P16 | P25 | P50 | P75 | P84 | 06d | 56d | Maximum |
|-------------------|---------|---------|----|-----|-----|-----|-----|-----|-----|-----|-----|---------|
| 1 | 49 | 15 | 28 | 31 | 35 | 38 | 45 | 59 | 66 | 70 | 77 | 100 |
| 2 | 53 | 10 | 25 | 32 | 33 | 40 | 52 | 65 | 71 | 75 | 80 | 100 |
| 3 | 50 | 15 | 24 | 32 | 35 | 39 | 49 | 60 | 65 | 71 | 77 | 100 |
| 4 | 35 | 10 | 13 | 13 | 16 | 19 | 30 | 45 | 52 | 60 | 69 | 100 |
| 5 | 31 | 13 | 13 | 15 | 16 | 17 | 27 | 39 | 46 | 53 | 65 | 100 |

Roundness, %

Table 4

| Powder particles elongation, % | | | | | | | | | | | | |
|--------------------------------|---------|---------|----|-----|-----|-----|-----|-----|-----|-----|-----|---------|
| Mixture number | Average | Minimum | P5 | P10 | P16 | P25 | P50 | 579 | P84 | 06d | P95 | Maximum |
| 1 | 33 | 0,01 | 11 | 14 | 17 | 22 | 32 | 45 | 50 | 51 | 54 | 91 |
| 2 | 34 | 0,01 | 10 | 14 | 17 | 21 | 32 | 44 | 49 | 54 | 59 | 91 |
| 3 | 39 | 0,01 | 12 | 15 | 21 | 26 | 40 | 49 | 55 | 59 | 64 | 92 |
| 4 | 39 | 0,01 | 10 | 16 | 22 | 29 | 38 | 51 | 57 | 61 | 64 | 97 |
| 5 | 38 | 0,01 | 12 | 16 | 20 | 27 | 37 | 51 | 53 | 58 | 65 | 93 |

Table 1



Fig. 1. Micrograph from microscope TESCAN VEGAII. Mixture No. 2, extension 100×

Comparison of average values of the mesh aperture diameter allows analyzing the ratio of dimensions of the compositions' particles. Adding binding, copper powder, coke, zinc stearate was done with simultaneous decrease of the graphite part in the composite and in the large decreased the average size of the composition particles. More than 50 % of particles in composition No. I have diameter less than 40 µm, when adding only 14 % of binding to the composition No. 2, there are more than 75 % of particles with the diameter less than 40 µm, thus, average diameter of the binding particles should be considerably less than 40 µm. Minimum and maximum values of the particles' diameter are not typical as minimum size is close to the granulo-morphometer sensitivity; the upper value is determined by the peculiarities of preparation of specimens for research.

Particles distribution by roundness is given in Table 3, by elongation – in Table 4. Roundness and elongation characterize the shape of particles of mixture components.

The photographs from the electron microscope (Fig. 1, 2), allow visually value the typical sizes and shape of the particles as well as the mixture homogeneity.

High Velocity Compaction research

The processes of High Velocity Compaction (HVC) carbon compositions were researched first of all scientists from ICSM of SUSU (Russia) in cooperation with scientists from National Engineering School in Saint-Etienne (France) [9–11] on the gas-hydraulic press HYP35–18¹ (Fig. 3).

¹ Hydropulsor AB. URL: http://www.hydropulsor.com



Fig. 2. Micrograph from microscope TESCAN VEGAII. Mixture No. 3, extension 1000×

Maximal striking energy of this press in 18 kJ, the strike speed can be changed within the range of 1-11 m/s. During experiments the striking energy varied within the range of 212-2247 J, this corresponds to the change of the punch speed which varied within the range of 1.10-3.58 m/s. Falling mass of the striker is equal to 350 kg.

Besides that, the processes of HVC were researched in Russia scientists from ICSM of SUSU on the CEAST 9350 produced by American Instron Engineering Corp.² in Italy with features: energy range 0.59–1800 J, impact speed 0.77–24 m/s, drop mass 2.0–70 kg. General view of the CEAST 9350 is given in Fig. 4. The CEAST 9350 is equipped wide range interchangeable falling masses available from 2.0 to 70 kg.

Fig. 5 presents a general view of the pressing block of high-speed gas-hydraulic press HYP 35-18, and Fig. 6 illustrates its principle of operation. The block works as follows. Powder is poured into the cavity of the press-mold and the punch is moved to its working position. High-speed pressing is begun by the action of a pulsator (indicated by the arrow) on the top punch. The pulsator in turn receives an energy pulse equal to 18 kNm by the discharge of an accumulator with high fluid pressure. The energy pulses can be changed within a range of 10-100 % of the maximum energy and the speed of the pulsator can be varied from 1 to 11 m/s. During operation in the pulsative forming regime, the shortest time between pulses is 450 ms.

² Instron Engineering Corp. URL: http://www.instron.ru

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Fig. 3. Press HYP 35-18 for HVC



Fig. 5. Pressing block of gas-hydraulic press HYP 35-18

Results of HVC research

Results of the research compacting from the graphite powder of cylindrical specimens are given in Table 5. Compacting energy values are



Fig. 4. The CEAST 9350



Fig. 6. Diagram showing the action of the forces during the forming operation

from 212 to 1892 J and punch stroking speed values are from 1.10 to 3.29 m/s. After compacting specimens 1 and 2 destroyed specimens 3 and 4 had defects in the form of delamination.





Table 5

| Specimen No. | Mixture Number | Specimen quantity | Energy, J | Speed, m/s | Specimen diameter, mm | Hight, mm | Density, g/cm ³ | | | |
|---|-------------------|----------------------|-----------|------------|--------------------------|---------------|----------------------------|--|--|--|
| Compaction from graphite powder | | | | | | | | | | |
| 1 | 1 | 1 | 212 | 1,10 | The s | specimen dest | royed | | | |
| 2 | 1 | 1 | 394 | 1,50 | The s | specimen dest | royed | | | |
| 3 | 1 | 1 | 1450 | 2,88 | 51,2 | 12,24 | 1,63 | | | |
| 4 | 1 | 1 | 1892 | 3,29 | 51,1 | 11,95 | 1,68 | | | |
| Compaction from mixture graphite + resin | | | | | | | | | | |
| 5 | 2 | 2 | 394 | 1,50 | 50,35 | 12,93 | 1,60 | | | |
| 6 | 2 | 1 | 632 | 1,90 | 50,34 | 12,75 | 1,62 | | | |
| 7 | 2 | 1 | 816 | 2,16 | 50,30 | 12,68 | 1,63 | | | |
| 8 | 2 | 1 | 1008 | 2,40 | 50,26 | 12,38 | 1,68 | | | |
| 9 | 2 | 1 | 1230 | 2,65 | 50,24 | 12,26 | 1,69 | | | |
| 10 | 2 | 1 | 1450 | 2,88 | 50,18 | 12,15 | 1,72 | | | |
| 11 | 2 | 1 | 1657 | 3,08 | 50,16 | 12,08 | 1,73 | | | |
| 12 | 2 | 1 | 1892 | 3,29 | 50,15 | 11,99 | 1,74 | | | |
| 13 | 2 | 2 | 2074 | 3,44 | 50,15 | 11,97 | 1,75 | | | |
| 14 | 2 | 5 | 2247 | 3,58 | 50,14 | 11,84 | 1,76 | | | |
| Compaction from mixture graphite + resin + copper | | | | | | | | | | |
| 15 | 3 | 1 | 1450 | 2,88 | 50,13 | 7,97 | 2,62 | | | |
| 16 | 3 | 1 | 1892 | 3,29 | 50,10 | 7,90 | 2,64 | | | |
| 17 | 3 | 1 | 2074 | 3,44 | 50,08 | 7,87 | 2,66 | | | |
| 18 | 3 | 3 | 2247 | 3,58 | 50,07 | 7,83 | 2,67 | | | |

Specimens compaction from the graphite powder and composition

After compacting specimens N_{2} 5–14 from compositions graphite + resin with the energy and speed values indicated in Table 5 no defects were found. When increasing the compaction energy and the punch stroke speed it is observed stable regularity of increasing density of the specimens from 1.60 to 1.76 g/cm³ (Fig. 7).



Fig. 8. Specimen from graphite + resin + copper powders

Compacting of the specimens from compositions graphite + resin + copper powders went without problems. The quality of the obtained specimens was high (Fig. 8).

Partial replacement of the graphite with coke powder did not lead to successful results. All 9 specimens obtained at formation energy 1892, 2074 and 2247 J and speed of 3.29, 3.44 and 3.58 m/s had some defects. Adding zinc stearate as a lubricant to the composite did not eliminate the defects.

Conclusions

Implementation of HVC will allow increasing the density, which in turn ensure the improved mechanical properties and decrease resistibility of such electrical products as trolleybuses current collectors, strips in pantograph collectors in trams, commuter rails, electric locomotives and brushes for electrical machines.

The increased velocity of formation leads to the increase of technical process operating efficiency at the given products formation.

The increase of work materials density after compaction makes it possible to reduce the part of the binding in the composition.

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ВЫСОКОСКОРОСТНОЕ КОМПАКТИРОВАНИЕ УГЛЕРОДНЫХ КОМПОЗИЦИЙ

М.Н. Самодурова, Л.А. Барков, Ю.С. Латфулина

Южно-Уральский государственный университет, г. Челябинск, Россия

Высокоскоростные процессы формования металлических, керамических и других порошков до сих пор не получили промышленного применения. Многочисленными попытками высокоскоростных формований порошков цветных, черных металлов, керамики и полимеров установлено, что формование при скоростях ударника, превышающих 1-2 м/с, сопровождаются такими неблагоприятными явлениями, как запрессовывание в формовках газов и паров жидкостей, содержащихся в исходных порошках, и разрушение формовок. В Челябинске имеется несколько крупных предприятий («Электродный завод», «Электрометаллургический комбинат», завод «Графитопласт», филиал «Донкарб графит», «Углеграфит», «Завод углеродных материалов» и др.), которые выпускают широкий ассортимент изделий из углеродных композиций. Ученые из Ресурсного центра специальной металлургии Южно-Уральского государственного университета (РЦСМ ЮУрГУ) провели теоретические, технологические и экспериментальные исследования для этих предприятий. Данная статья посвящена анализу выполненных экспериментальных исследований на устройствах шведской фирмы HYDROPULSOR и американской фирмы Instron. Зарубежными исследователями установлены значения кинетической энергии бойков устройств, при которых плотность формовок приближается к теоретической, но без указания составов порошков и характера уплотнения формовок, а также массы бойков и формовок, их плотности при различных значениях скоростей и массы бойков. Таким образом, задача работы состояла в исследовании высокоскоростного

формования разных составов композиций на основе графита при оптимальной массе бойков устройств и формовок, а также оптимальной скорости бойков устройств.

Ключевые слова: высокоскоростное формование; углеродные композиции; грануло-морфологические исследования; прессы HYDROPULSOR.

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Самодурова Марина Николаевна, канд. техн. наук, доцент кафедры машин и технологий обработки материалов давлением, руководитель Ресурсного центра спецметаллургии, Южно-Уральский государственный университет, г. Челябинск; samodurovamn@susu.ru.

Барков Леонид Андреевич, д-р техн. наук, профессор, заместитель по научной работе руководителя Ресурсного центра спецметаллургии, Южно-Уральский государственный университет, г. Челябинск; barkovla@susu.ru.

Латфулина Юлия Сергеевна, инженер-исследователь Ресурсного центра спецметаллургии, Южно-Уральский государственный университет, г. Челябинск; latfulina174@gmail.com.

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